

Order by order

(2)

$$\mathcal{O}(\frac{1}{\varepsilon}): 0 = C(f_0, f_0) \Rightarrow f_0 = f^{\text{eq}}$$

$$\mathcal{O}(1): \partial_{\vec{q}} f_0 + \mathcal{L}_1 f_0 = C(f_0, f_1) + C(f_1, f_0)$$

Leading order & slow fields

$$f_0(\vec{q}, \vec{p}, t) = \tilde{f}(\vec{q}, t) e^{-\vec{\alpha}(\vec{q}, t) \cdot \vec{p} - \beta(\vec{q}, t) \left[\frac{\vec{p}^2}{2m} + U(\vec{q}) \right]}$$

Can we parametrize f_0 in terms of the conserved fields?

density $n(\vec{q}, t) = \int d\vec{p} f(\vec{q}, \vec{p}, t) \quad (d)$

momentum $\vec{w}(\vec{q}, t) = \int d\vec{p} \vec{p} f(\vec{q}, \vec{p}, t) \quad (m)$

kinetic energy $\kappa(\vec{q}, t) = \int d\vec{p} \frac{\vec{p}^2}{2m} f(\vec{q}, \vec{p}, t) \quad (h)$

In principle, $n = n_0 + \varepsilon n_1 + \varepsilon^2 n_2, \vec{w} = \vec{w}_0 + \varepsilon \vec{w}_1 + \varepsilon^2 \vec{w}_2 + \dots$

$$\kappa = \kappa_0 + \varepsilon \kappa_1 + \varepsilon^2 \kappa_2$$

(d, m, h), to order 0, show that n_0, \vec{w}_0 & κ_0 determine entirely

f_0 , which is a Gaussian function, hence entirely determined by

its normalization & two first moments.

To determine the evolution of f_0 , we can thus use the evolution

of n, \vec{w} & $\kappa \Rightarrow$ let's build them!

2.4.2) The hydrodynamic equations

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Evolution of the density field

$$n(\vec{q}) = \int d^3 \vec{p}_i f(\vec{q}, \vec{p}_i) \Rightarrow \int d^3 \vec{p}_i (BE) \text{ gives}$$

$$\partial_t n + \frac{\partial}{\partial \vec{q}} \cdot \int d^3 \vec{p}_i f \frac{\vec{p}_i}{m} = \int d^3 \vec{p}_1 d^3 \vec{p}_2 d^2 \sigma |\vec{v}_1 - \vec{v}_2| (f_1' f_2' - f_1 f_2) \times 1$$

(symmetrize the r.h.s by doing $\vec{p}_1 \leftrightarrow \vec{p}_2$ & then
 $(\vec{p}_1, \vec{p}_2) \leftrightarrow (\vec{p}_1', \vec{p}_2')$)

$$\partial_t n + \frac{\partial}{\partial \vec{q}} \cdot j(\vec{q}) = \frac{1}{4} \int d^3 \vec{p}_1 d^3 \vec{p}_2 d^2 \sigma |\vec{v}_1 - \vec{v}_2| (f_1' f_2' - f_1 f_2) \left[\overbrace{1+1-1-1}^{\substack{\vec{p}_1 \leftrightarrow \vec{p}_2 \\ \vec{p}_1 \leftrightarrow \vec{p}_1' \\ =0}} \right]$$
$$j(\vec{q}) = \int d^3 \vec{p} \vec{v} f(\vec{q}, \vec{p}, t)$$

$$\Leftrightarrow \boxed{\partial_t n + \frac{\partial}{\partial \vec{q}} \cdot j(\vec{q}) = 0} \quad \text{local conservation law}$$

Velocity field: $f(\vec{q}, \vec{p}, t)$ is locally proportional to the number of particles \Rightarrow so is $j(\vec{q})$, one thus defines a local velocity field as $j(\vec{q}, t) \equiv n(\vec{q}, t) \vec{u}(\vec{q}, t)$

This can be rewritten as

$$\boxed{\vec{u}(\vec{q}, t) = \frac{\int d^3 \vec{p} \vec{v} f(\vec{q}, \vec{p}, t)}{\int d^3 \vec{p} f(\vec{q}, \vec{p}, t)} = \langle \vec{v} \rangle_{f, \vec{q}}}$$

where $\langle O(\vec{p}) \rangle_{f, \vec{q}} = \int d^3 \vec{p} O(\vec{p}) f_{f, \vec{q}}(\vec{p})$

and $f_{f, \vec{q}} = \frac{f(\vec{q}, \vec{p}, t)}{\int d^3 \vec{p} f(\vec{q}, \vec{p}, t)}$ is the conditional probability density that a particle at \vec{q} has momentum \vec{p} .

To lighten notation, in this chapter we drop the subscript

$$\langle \dots \rangle_{f, \vec{q}} \rightarrow \langle \dots \rangle$$

Evolution equation for the density field

$$\partial_t m(\vec{q}, t) = - \frac{\partial}{\partial \vec{q}} \cdot [\vec{u}(\vec{q}, t) m(\vec{q}, t)] \quad (1)$$

Material derivatives

$$(1) \Leftrightarrow \partial_t \vec{u} + \vec{u} \cdot \frac{\partial}{\partial \vec{q}} \vec{u} = - m \frac{\partial}{\partial \vec{q}} \cdot \vec{u}$$

$$\Leftrightarrow D_t \vec{u}(\vec{q}, t) = - m \frac{\partial}{\partial \vec{q}} \cdot \vec{u} = - m \partial_{q_\alpha} u_\alpha \quad (1')$$

where $D_t = \frac{\partial}{\partial t} + \vec{u} \cdot \frac{\partial}{\partial \vec{q}} = \frac{\partial}{\partial t} + u_\alpha \frac{\partial}{\partial q_\alpha}$ is the material derivative

and summations over repeated indices are implicit.

(1) is nice but not closed \Rightarrow dynamics of \vec{u}

Evolution of the velocity field

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$$u_\alpha = \frac{1}{n} \int dp v_\alpha f$$

$$\partial_t u_\alpha = - \frac{\partial \epsilon^n}{n^2} \underbrace{\int dp v_\alpha f}_{n u_\alpha} + \frac{1}{n} \int dp v_\alpha \partial_t f$$

$$= \frac{\partial q_\beta (u_\beta n)}{n} u_\alpha + \frac{1}{n} \int dp v_\alpha [-v_\beta \partial_{q_\beta} f] + \frac{1}{n} \int dp_1 dp_2 d\sigma |\vec{v}_1 - \vec{v}_2| (f_1' f_2' - f_1 f_2) v_{1,\alpha}$$

↓ symmetrization

$$= u_\alpha \partial_{q_\beta} u_\beta + \frac{u_\alpha u_\beta}{n} \partial_{q_\beta} n - \frac{1}{n} \partial_{q_\beta} \int dp v_\alpha v_\beta f + \frac{1}{4n} \int dp_1 dp_2 |\vec{v}_1 - \vec{v}_2| (f_1' f_2' - f_1 f_2) (v_{1,\alpha} + v_{2,\alpha} - v_{1',\alpha} - v_{2',\alpha})$$

= 0 since $\vec{p}_{CM} = \vec{p}_{CM}'$
 \Rightarrow true for any collisional invariant

$$D_t u_\alpha = \partial_t u_\alpha + u_\beta \partial_{q_\beta} u_\alpha = \partial_{q_\beta} (u_\alpha u_\beta) + \frac{u_\alpha u_\beta}{n} \partial_{q_\beta} n - \frac{1}{n} \partial_{q_\beta} (n \langle v_\alpha v_\beta \rangle)$$

$\underbrace{\qquad\qquad\qquad}_{\frac{1}{n} \partial_{q_\beta} (n u_\alpha u_\beta)}$

$$D_t u_\alpha = - \frac{1}{n} \partial_{q_\beta} \left[n \underbrace{(\langle v_\alpha v_\beta \rangle - \langle v_\alpha \rangle \langle v_\beta \rangle)}_{\langle \underbrace{(v_\alpha - \langle v_\alpha \rangle)}_{\delta v_\alpha} \underbrace{(v_\beta - \langle v_\beta \rangle)}_{\delta v_\beta} \rangle} \right] = - \frac{1}{n} \partial_{q_\beta} [n \langle v_\alpha v_\beta \rangle_c]$$

This suggests introducing the pressure tensor

$$P_{\alpha\beta} = n m \langle (v_\alpha - u_\alpha) (v_\beta - u_\beta) \rangle = n m \langle \delta v_\alpha \delta v_\beta \rangle$$

which yields

$$n D_t u_\alpha = - \frac{1}{n} \partial_{q_\beta} \cdot P_{\alpha\beta} \Leftrightarrow n D_t \vec{u} = - \frac{1}{n} \vec{\nabla} \cdot \vec{P} \quad (2)$$

Comments: * (1) & (2) are like the Navier Stokes equations for a gas.

⑥

* To close (1) & (2) to order ε^0 , we need to compute $p_{\alpha\beta}$ & thus know f^0 . We still miss the second moment of \vec{p} to do that.

Evolution of the kinetic energy:

$$\varepsilon = \left\langle \frac{1}{2} m \delta \vec{v}^2 \right\rangle = \frac{1}{2} m \left(\langle \vec{v}^2 \rangle - \vec{u}^2 \right)$$

Painful algebra leads to:

$$\partial_t \varepsilon + u_\alpha \partial_{q_\alpha} \varepsilon = -\frac{1}{m} \partial_\alpha h_\alpha - \frac{1}{m} p_{\alpha\beta} u_{\alpha\beta} \quad (3)$$

where:

* $u_{\alpha\beta} = \frac{1}{2} (\partial_{q_\alpha} u_\beta + \partial_{q_\beta} u_\alpha)$ is the strain rate tensor

* $h_\alpha = \frac{m}{2} \langle \delta v_\alpha \delta v_\beta \delta v_\beta \rangle$ is the kinetic energy flux
also called heat flux

$$\Leftrightarrow \vec{h} = \frac{m}{2} \langle \delta \vec{v} \|\delta \vec{v}\|^2 \rangle$$

Proof of Eq (3):

$$\partial_t (m\varepsilon) = \frac{1}{2} m \partial_t \int d^3\vec{p} f (\vec{v} - \vec{u})^2$$

$$= \underbrace{\frac{m}{2} \int d^3\vec{p} (\vec{v} - \vec{u})^2 \partial_t f}_{(2)} + \underbrace{m \int d^3\vec{p} f (\vec{u} - \vec{v}) \partial_t \vec{u}}_{(1)}$$

$$\textcircled{1} = m \partial_{\epsilon} \mu \left[\underbrace{\vec{u} \int d^3 \vec{p} f}_{=1} - \underbrace{\int d^3 \vec{p} f \vec{v}}_{=\vec{u}} \right] = 0$$

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$$\textcircled{2} = \frac{m}{2} \int d^3 \vec{p} (\vec{v} \cdot \vec{u})^2 \left[-\vec{v} \cdot \frac{\partial}{\partial \vec{r}} f + \int d^3 \vec{p}' d\tau |\vec{r} - \vec{r}_2| (f' f'_2 - f f_2) \right]$$

leads to 0 because \vec{v}^2 is a collisional invariant

$$\begin{aligned} \Rightarrow \textcircled{2} &= -\frac{m}{2} \frac{\partial}{\partial q_{\alpha}} \cdot \left[\int d^3 \vec{p} \delta \vec{v}^2 v_{\alpha} f \right] + \frac{m}{2} \int d^3 \vec{p} v_{\alpha} f \underbrace{\frac{\partial}{\partial q_{\alpha}} \delta \vec{v}^2}_{2(\mu_{\beta} \cdot \tau_{\beta}) \frac{\partial}{\partial q_{\alpha}} \mu_{\beta}} \\ &= -\partial_{q_{\alpha}} \left[\frac{m}{2} \langle \delta \vec{v}^2 v_{\alpha} \rangle \right] + m (\partial_{q_{\alpha}} \mu_{\beta}) \underbrace{\int d^3 \vec{p} f v_{\alpha} (\mu_{\beta} - v_{\beta})}_{=0} \\ &= \underbrace{\int d^3 \vec{p} f (v_{\alpha} - \mu_{\alpha}) (\mu_{\beta} - v_{\beta})}_{= \frac{P_{\alpha\beta}}{m}} + \underbrace{\mu_{\alpha} \int d^3 \vec{p} f (v_{\beta} - v_{\beta})}_{=0} \end{aligned}$$

$$\Rightarrow \partial_{\epsilon} (m \epsilon) = -\partial_{q_{\alpha}} \left[\frac{m}{2} \langle \delta \vec{v}^2 v_{\alpha} \rangle \right] - (\partial_{q_{\alpha}} \mu_{\beta}) P_{\alpha\beta}$$

$$= m \partial_{\epsilon} \epsilon + \epsilon \partial_{\epsilon} m = m \partial_{\epsilon} \epsilon - \epsilon \partial_{q_{\alpha}} (m \mu_{\alpha}) = m \partial_{\epsilon} \epsilon - \partial_{q_{\alpha}} (m \epsilon \mu_{\alpha}) + m \mu_{\alpha} \partial_{q_{\alpha}} \epsilon$$

$$\Rightarrow m \partial_{\epsilon} \epsilon + m \mu_{\alpha} \partial_{q_{\alpha}} \epsilon = -\partial_{q_{\alpha}} \left[\frac{m}{2} \langle \delta \vec{v}^2 v_{\alpha} \rangle - \frac{m}{2} \langle \delta \vec{v}^2 \mu_{\alpha} \rangle \right] - P_{\alpha\beta} \mu_{\alpha\beta}$$

$$\begin{aligned} \text{when we used } (\partial_{q_{\alpha}} \mu_{\beta}) P_{\alpha\beta} &= \frac{1}{i} \left[\partial_{q_{\alpha}} \mu_{\beta} P_{\alpha\beta} + \partial_{q_{\beta}} \mu_{\alpha} \overbrace{P_{\beta\alpha}}^{=P_{\alpha\beta}} \right] = P_{\alpha\beta} \frac{1}{2} (\partial_{q_{\alpha}} \mu_{\beta} + \partial_{q_{\beta}} \mu_{\alpha}) \\ &= P_{\alpha\beta} \mu_{\alpha\beta} \end{aligned}$$

$$\text{All in all, } \partial_{\epsilon} \epsilon + \mu_{\alpha} \partial_{q_{\alpha}} \epsilon = -\frac{1}{m} \partial_{q_{\alpha}} \left[\frac{m}{2} \langle \delta \vec{v}^2 \delta v_{\alpha} \rangle \right] - \frac{1}{m} P_{\alpha\beta} \mu_{\alpha\beta} \quad \Rightarrow \text{Eq (3)}$$

Temperature field

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It is useful to define $T(\vec{q}, t) = \frac{2}{3} \frac{\varepsilon(\vec{q}, t)}{k_B}$ such that $\varepsilon = \frac{3}{2} k_B T$ and

$$\partial_t T + u_\alpha \partial_\alpha T = -\frac{2}{3mk_B} \partial_\alpha h_\alpha - \frac{2}{3mk_B} \rho_{\alpha\beta} u_{\alpha\beta}$$

Closure: We can now close everything to order ε^0 .

We can use n, u, T to order ε^0 to characterize f_0 & f_0 to compute P_0 & h_0

which in turn close the dynamics for n, u, T to order ε^0 .

Notation: $A_0 \sim A^0$ refers to the observable A at order ε^0 .

2.4.3) leading order dynamics

Given n_0, T_0, \vec{u}_0 , we determine f_0 through

$$\int f_0 d\vec{p} = n_0$$

$$\int \vec{v} f_0 d\vec{p} = \vec{u}_0$$

$$\int \frac{m}{2} (\vec{v} - \vec{u}_0)^2 f_0 d\vec{p} = n_0(\vec{q}) \varepsilon_0(\vec{q}) \\ = \frac{3}{2} n_0 k_B T_0(\vec{q})$$

$$f_0(\vec{q}, \vec{p}, t) = \frac{n_0(\vec{q}, t)}{(2\pi m k_B T_0(\vec{q}, t))^{3/2}} e^{-\frac{[\vec{p} - m\vec{u}(\vec{q}, t)]^2}{2 m k_B T_0(\vec{q}, t)}} \\ = \frac{n_0}{(2\pi m k_B T_0)^{3/2}} e^{-\frac{m \delta \vec{v}^2}{2 k_B T_0}}$$

Pressure & heat flux

$$P_{\alpha\beta}^0 = n_0 m \langle \delta v_\alpha \delta v_\beta \rangle_0 = m \frac{n_0 k_B T_0}{m} \delta_{\alpha\beta} = n_0 k_B T_0 \delta_{\alpha\beta}$$

The pressure is isotropic and obeys the ideal gas law!

$h_\alpha^0 \propto \langle \delta v^2 \delta v_\alpha \rangle = 0$ since it involves an odd of a Gaussian.

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leading order dynamics

$$\partial_t n_0 + \vec{u}_0 \cdot \vec{\nabla} n_0 = -n_0 \vec{\nabla} \cdot \vec{u}_0 \quad (1)$$

$$m \left[\partial_t \vec{u}_0 + \vec{u}_0 \cdot \vec{\nabla} \vec{u}_0 \right] = -\frac{1}{m} \vec{\nabla} \cdot (n_0 k_B T) \quad (2)$$

$$\partial_t T_0 + \vec{u}_0 \cdot \vec{\nabla} T_0 = -\frac{2}{3} T_0 \vec{\nabla} \cdot \vec{u}_0 \quad (3)$$

To order ϵ^0 , $f = f^0$ is left invariant by collisions, but transport occurs due to $\{f, H\}$, which leads to slow evolution of n_0, \vec{u}_0, T_0 .

Is it enough to equilibrate?